

Amendments to the Claims:

This listing of claims will replace all prior versions, and listings, of claims in the application:

Listing of Claims:

1. (Canceled)

2. (Currently Amended) ~~-A charge rate estimating apparatus for a secondary cell as claimed in claim 1,~~ A charge rate estimating apparatus for a secondary cell, comprising:

a current detecting section capable of measuring a current flowing through the secondary cell;

a terminal voltage detecting section capable of measuring a voltage across terminals of the secondary cell;

a parameter estimating section that calculates an adaptive digital filtering using a cell model in a continuous time series shown in an equation (1) and estimates all parameters at one time, the parameters corresponding to an open-circuit voltage V_0 which is an offset term of the equation (1) and coefficients of $A(s)$, $B(s)$, and $C(s)$, which are transient terms; and

a charge rate estimating section that estimates the charge rate from a previously derived relationship between an open-circuit voltage and a charge rate of the secondary cell and the open-circuit voltage V_0 ,

$$V = \frac{B(s)}{A(s)} \cdot I + \frac{1}{C(s)} \cdot V_0 \text{ --- (1), wherein } s \text{ denotes a Laplace}$$

transform operator, $A(s)$, $B(s)$, and $C(s)$ denote poly-nominal functions of s ,

wherein the open-circuit voltage V_0 of the cell model in the continuous time series shown in the equation (1) is

approximated by means of an equation (2) to provide an equation (3) and the adaptive digital filter calculation is carried out using the equation (3) and equivalent equation (4), h is estimated in at least equation (4), the estimated h is substituted into equation (2) to derive an open-circuit voltage V_0 , ~~and the charge rate is estimated from a relationship between the previously derived open-circuit voltage V_0 , and the charge rate is estimated from a the previously derived relationship between an open-circuit voltage and a charge rate of the secondary cell and the previously proposed open-circuit voltage V_0 and the charge rate (SOC) open-circuit voltage V_0 .~~

$$V_0 = \frac{h}{s} \cdot I \quad \text{--- (2)}$$

$$V = \left(\frac{B(s)}{A(s)} + \frac{1}{C(s)} \cdot \frac{h}{s} \right) \cdot I = \frac{s \cdot B(s) \cdot C(s) + h \cdot A(s)}{s \cdot A(s) \cdot C(s)} \cdot I \quad \text{--- (3)}$$

$$\frac{s \cdot A(s) \cdot C(s)}{G_1(s)} \cdot V = \frac{s \cdot B(s) \cdot C(s) + h \cdot A(s)}{G_1(s)} \cdot I \quad \text{---- (4), wherein } s$$

denotes the Laplace transform operator, $A(s)$, $B(s)$, and $C(s)$ denote poly-nominal equation functions, h denotes a variable, and $1/G_1(s)$ denotes a transfer function having a low pass filter characteristic.

3. (Currently Amended) ~~A charge rate estimating apparatus for a secondary cell as claimed in claim 1, A charge rate estimating apparatus for a secondary cell, comprising:~~

a current detecting section capable of measuring a current flowing through the secondary cell;

a terminal voltage detecting section capable of measuring a voltage across terminals of the secondary cell;

a parameter estimating section that calculates an adaptive digital filtering using a cell model in a continuous time series shown in an equation (1) and estimates all parameters at one time, the parameters corresponding to an open-circuit voltage V_0 , which is an offset term of the equation (1), and coefficients of $A(s)$, $B(s)$, and $C(s)$, which are transient terms; and

a charge rate estimating section that estimates the charge rate from a previously derived relationship between an open-circuit voltage and a charge rate of the secondary cell and the open-circuit voltage V_0 ,

$$\underline{V = \frac{B(s)}{A(s)} \cdot I + \frac{1}{C(s)} \cdot V_0} \text{ --- (1), wherein } s \text{ denotes a Laplace}$$

transform operator, $A(s)$, $B(s)$, and $C(s)$ denote poly-nominal functions of s ,

wherein the open-circuit voltage V_0 of the cell model in the time continuous time series is approximated in an equation (2) to calculate an equation (3), the adaptive digital filter calculation is carried out using an equation (4) which is equivalent to the equation (3), $A(s)$, $B(s)$, and $C(s)$ are estimated from equation (4), the estimated $A(s)$, $B(s)$, and $C(s)$ are substituted into equation (5) to determine $V_0/G_2(s)$ and the charge rate is estimated from the previously derived relationship between an open-circuit voltage and a charge rate of the secondary cell and the~~previously derived open-circuit voltage V_0 and the charge rate (SOC)~~ using the derived $V_0/G_2(s)$ in place of the open-circuit voltage V_0 ,

$$V_0 = \frac{h}{s} \cdot I \text{ --- (2)}$$

$$V = \left(\frac{B(s)}{A(s)} + \frac{1}{C(s)} \cdot \frac{h}{s} \right) \cdot I = \frac{s \cdot B(s) \cdot C(s) + h \cdot A(s)}{s \cdot A(s) \cdot C(s)} \cdot I \quad \text{--- (3)}$$

$$\frac{s \cdot A(s) \cdot C(s)}{G_1(s)} \cdot V = \frac{s \cdot B(s) \cdot C(s) + h \cdot A(s)}{G_1(s)} \cdot I \quad \text{---- (4),}$$

$\frac{V_0}{G_2(s)} = \frac{C(s)}{G_2(s)} \cdot \left(V - \frac{B(s)}{A(s)} \cdot I \right)$ --- (5), wherein s denotes the Laplace transform operator, $A(s)$, $B(s)$, and $C(s)$ denote the polynomial (equation) function of s , h denotes a variable, $1/G_1(s)$ and $1/G_2(s)$ denote transfer functions having the low pass filter characteristics.

4. (Currently Amended) A charge rate estimating apparatus for a secondary cell as claimed in claim 1, wherein the cell model is calculated from an equation (6),

$$V = \frac{K \cdot (T_2 \cdot s + 1)}{T_1 \cdot s + 1} \cdot I + \frac{1}{T_3 \cdot s + 1} V_0, \text{ wherein } K \text{ denotes an internal resistance of the secondary cell, } T_1, T_2, \text{ and } T_3 \text{ denote time constants and, } 1/G_1(s) \text{ denotes a low pass filter having a third order or more, and } 1/G_2(s) \text{ denotes another low pass filter having a second order or more wherein } A(s) = T_1 \cdot s + 1, B(s) = K \cdot (T_2 \cdot s + 1), C(s) = T_3 \cdot s + 1.$$

5. (Canceled)

6. (Currently Amended) A charge rate estimating apparatus for a secondary cell as claimed in ~~claim 5~~ claim 4, wherein

$$V = \frac{K \cdot (T_2 \cdot s + 1)}{T_1 \cdot s + 1} \cdot I + \frac{1}{T_3 \cdot s + 1} \cdot \frac{A}{s} \cdot I \quad \text{---- (9)}$$

$$(a \bullet s^3 + b \bullet s^2 + s) \bullet V = (c \bullet s^3 + d \bullet s^2 + e \bullet s + f) \bullet I \text{ --- (10).}$$

7. (Original) A charge rate estimating apparatus for a secondary cell as claimed in claim 6, wherein $a = T_1 \bullet T_3$, $b = T_1 + T_3$, $c = K \bullet T_2 \bullet T_3$, $d = K \bullet (T_2 + T_3)$, $e = K + A \bullet T_1$, $f = A$ --- (11).

8. (Original) A charge rate estimating apparatus for a secondary cell as claimed in claim 7, wherein a stable low pass filter $G_1(s)$ is introduced into both sides of the equation (10) to derive the following equation:

$$\frac{1}{G_1(s)} (a \bullet s^3 + b \bullet s^2 + s) \bullet V = \frac{1}{G_1(s)} (c \bullet s^3 + d \bullet s^2 + e \bullet s + f) \bullet I \text{ --- (12).}$$

9. (Currently Amended) A charge rate estimating apparatus for a ~~Secondary~~ secondary cell as claimed in claim 8, wherein actually measurable currents I and terminal voltages V which are processed by means of a low pass filter are as follows:

$$\begin{aligned} I_0 &= \frac{1}{G_1(s)} \bullet I, \\ I_1 &= \frac{s}{G_1(s)} \bullet I, & V_1 &= \frac{s}{G_1(s)} \bullet V, \\ I_2 &= \frac{s^2}{G_1(s)} \bullet I, & V_2 &= \frac{s^2}{G_1(s)} \bullet V, \\ I_3 &= \frac{s^3}{G_1(s)} \bullet I, & V_3 &= \frac{s^3}{G_1(s)} \bullet V, \text{ and} \\ \frac{1}{G_1(s)} &= \frac{1}{(P_1 \bullet s + 1)^3} \text{ --- (13).} \end{aligned}$$

10. (Currently Amended) A charge rate estimating apparatus for a

secondary cell as claimed in claim 9, wherein, using the equation (13), the equation of (12) is rewritten and rearranged as follows:

$$V_1 = [V_3 \quad V_2 \quad I_3 \quad I_2 \quad I_1 \quad I_0] \cdot \begin{bmatrix} -a \\ -b \\ c \\ d \\ e \\ f \end{bmatrix} \quad \text{--- (15) and}$$

the equation (15) corresponds to a general equation which is coincident with a standard form of a general adaptive digital filter of equation (16): $y = \omega^T \cdot \theta$ --- (16), wherein $y = V_1$, $\omega^T = [V_3 \quad V_2 \quad I_3 \quad I_2 \quad I_1 \quad I_0]$, and

$$\theta = \begin{bmatrix} -a \\ -b \\ c \\ d \\ e \\ f \end{bmatrix} \quad \text{--- (17).}$$

11. (Currently Amended) A charge rate estimating apparatus for a

Secondary cell as claimed in claim 10, wherein a parameter estimating algorithm with the equation (16) as a prerequisite is defined as follows:

$$\gamma(k) = \frac{\lambda_3(k)}{1 + \lambda_3(k) \cdot \omega^T(k) \cdot P(k-1) \cdot \omega(k)}$$

$$\theta(k) = \theta(k-1) - \gamma(k) \cdot P(k-1) \cdot \omega(k) \cdot [\omega^T(k) \cdot \theta(k-1) - y(k)]$$

$$P(k) = \frac{1}{\lambda_1(k)} \left\{ P(k-1) - \frac{\lambda_3(k) \cdot P(k-1) \cdot \omega(k) \cdot \omega^T(k) \cdot P(k-1)}{1 + \lambda_3(k) \cdot \omega^T(k) \cdot P(k-1) \cdot \omega(k)} \right\} = \frac{P'(k)}{\lambda_1(k)}$$

$$\lambda_1(k) = \left\{ \begin{array}{l} \cancel{*} \frac{\text{trace}\{P'(k)\}}{\gamma_U} : \lambda_1 \leq \frac{\text{trace}\{P'(k)\}}{\gamma_U} \\ \cancel{*} \lambda_1 : \frac{\text{trace}\{P'(k)\}}{\gamma_U} \leq \lambda_1 \leq \frac{\text{trace}\{P'(k)\}}{\gamma_L} \\ \cancel{*} \frac{\text{trace}\{P'(k)\}}{\gamma_L} : \frac{\text{trace}\{P'(k)\}}{\gamma_L} \leq \lambda_1 \end{array} \right.$$

----- (18),

wherein $\theta(k)$ denotes a parameter estimated value at a time point of k ($k = 0, 1, 2, 3 \dots$), λ_1 , $\lambda_3(k)$, γ_U , and γ_L denote initial set value, $b < \lambda_1 < 1$, $0 < \lambda_3(k) < \infty$, $P(0)$ is a ~~sufficiently large value~~, of $P(k)$ at $k=0$, $\theta(0)$ is $\theta(k)$ at $k=0$ and $\theta(0)$ provides an initial value which is non-zero ~~but very~~ ~~sufficiently small value~~, and $\text{trace}\{P\}$ means a trace of matrix P .

12. (Canceled)

13. (Currently Amended) ~~A charge rate estimating method for a secondary cell as claimed in claim 12,~~ A charge rate estimating method for a secondary cell, comprising:

measuring a current flowing through the secondary cell;
measuring a voltage across terminals of the secondary cell;

calculating an adaptive digital filtering to provide an adaptive digital filter calculation using a cell model in a continuous time series shown in an equation (1);

estimating all parameters at one time, the parameters corresponding to an open-circuit voltage V_0 , which is an offset term of the equation (1), and coefficients of $A(s)$, $B(s)$, and $C(s)$, which are transient terms; and

estimating the charge rate from a previously derived relationship between an open-circuit voltage and a charge rate of the secondary cell and the open-circuit voltage V_0 ,

$$V = \frac{B(s)}{A(s)} \cdot I + \frac{1}{C(s)} \cdot V_0 \quad \text{--- (1), wherein } s \text{ denotes a Laplace}$$

transform operator, $A(s)$, $B(s)$, and $C(s)$ denote poly-nominal functions of s ,

wherein the open-circuit voltage V_0 of the cell model in the continuous time series shown in the equation (1) is approximated by means of an equation (2) to provide an equation (3) and the adaptive digital filter calculation is carried out using the equation (3) and equivalent equation (4), h is estimated in at least equation (4), the estimated value of h is substituted into equation (2) to derive an open-circuit voltage V_0 , ~~and the charge rate is estimated from a relationship between the previously derived open-circuit voltage V_0 , and the charge rate is estimated from a~~ previously derived relationship between the previously proposed an open-circuit voltage and a charge rate of the secondary cell and the open-circuit voltage V_0 and the charge rate (SOC).

$$V_0 = \frac{h}{s} \cdot I \quad \text{--- (2)}$$

$$V = \left(\frac{B(s)}{A(s)} + \frac{1}{C(s)} \cdot \frac{h}{s} \right) \cdot I = \frac{s \cdot B(s) \cdot C(s) + h \cdot A(s)}{s \cdot A(s) \cdot C(s)} \cdot I \quad \text{--- (3)}$$

$$\frac{s \cdot A(s) \cdot C(s)}{G_1(s)} \cdot V = \frac{s \cdot B(s) \cdot C(s) + h \cdot A(s)}{G_1(s)} \cdot I \quad \text{---- (4), wherein } s$$

denotes the Laplace transform operator, $A(s)$, $B(s)$, and $C(s)$ denote poly-nominal equation functions, h denotes a variable,

and $1/G_1(s)$ denotes a transfer function having a low pass filter characteristic.

14. (Currently Amended) ~~A charge rate estimating method for a secondary cell as claimed in claim 12,~~ A charge rate estimating method for a secondary cell, comprising:

measuring a current flowing through the secondary cell;
measuring a voltage across terminals of the secondary cell;

calculating an adaptive digital filtering to provide an adaptive digital filter calculation using a cell model in a continuous time series shown in an equation (1);

estimating all parameters at one time, the parameters corresponding to an open-circuit voltage V_0 , which is an offset term of the equation (1), and coefficients of $A(s)$, $B(s)$, and $C(s)$, which are transient terms; and

estimating the charge rate from a previously derived relationship between an open-circuit voltage and a charge rate of the secondary cell and the open-circuit voltage V_0 ,

$$V = \frac{B(s)}{A(s)} \cdot I + \frac{1}{C(s)} \cdot V_0 \text{ --- (1), wherein } s \text{ denotes a Laplace}$$

transform operator, $A(s)$, $B(s)$, and $C(s)$ denote poly-nominal functions of s ,

wherein the open-circuit voltage V_0 of the cell model in the continuous time series is approximated in an equation (2) to calculate an equation (3), the adaptive digital filter calculation is carried out using an equation (4) which is equivalent to the equation (3), $A(s)$, $B(s)$, and $C(s)$ are estimated from the equation (4), the estimated $A(s)$, $B(s)$, and $C(s)$ are substituted into equation (5) to determine $V_0/G_2(s)$ and the charge rate is estimated ~~from the~~ from the previously

derived relationship between an open-circuit voltage and a charge rate of the secondary cell, and the previously derived the open-circuit voltage V_0 and the charge rate $\{SOC\}$ using the derived $V_0/G_2(s)$ in place of the open-circuit voltage V_0 ,

$$V_0 = \frac{h}{s} \cdot I \quad \text{--- (2)}$$

$$V = \left(\frac{B(s)}{A(s)} + \frac{1}{C(s)} \cdot \frac{h}{s} \right) \cdot I = \frac{s \cdot B(s) \cdot C(s) + h \cdot A(s)}{s \cdot A(s) \cdot C(s)} \cdot I \quad \text{--- (3)}$$

$$\frac{s \cdot A(s) \cdot C(s)}{G_1(s)} \cdot V = \frac{s \cdot B(s) \cdot C(s) + h \cdot A(s)}{G_1(s)} \cdot I \quad \text{---- (4),}$$

$\frac{V_0}{G_2(s)} = \frac{C(s)}{G_2(s)} \cdot (V - \frac{B(s)}{A(s)} \cdot I)$ --- (5), wherein s denotes the Laplace transform operator, $A(s)$, $B(s)$, and $C(s)$ denote the polynomial (equation) function of s , h denotes a variable, $1/G_1(s)$ and $1/G_2(s)$ denote transfer functions having the low pass filter characteristics.

15. (Currently Amended) A charge rate estimating method for a secondary cell as claimed in ~~claim 12~~ claim 13, wherein the cell model is calculated from an equation (6), $[[.]]$

$$V = \frac{K \cdot (T_2 \cdot s + 1)}{T_1 \cdot s + 1} \cdot I + \frac{1}{T_3 \cdot s + 1} V_0, \text{ wherein } K \text{ denotes an internal}$$

resistance of the secondary cell, T_1 , T_2 , and T_3 denote time constants, $1/G_1(s)$ denotes a low pass filter having a third order or more, ~~and $1/G_2(s)$ denotes another low pass filter having a second order or more.~~

16.-18. (Canceled)

19. (New) A charge rate estimating apparatus for a secondary cell as claimed in claim 3, wherein the cell model is calculated from an equation (6),

$$V = \frac{K \cdot (T_2 \cdot s + 1)}{T_1 \cdot s + 1} \cdot I + \frac{1}{T_3 \cdot s + 1} V_0$$

wherein K denotes an internal resistance of the secondary cell, T_1 , T_2 , and T_3 denote time constants, $1/G_1(s)$ denotes a low pass filter having a third order or more, and $1/G_2(s)$ denotes another low pass filter having a second order or more, wherein $A(s) = T_1 \cdot s + 1$, $B(s) = K \cdot (T_2 \cdot s + 1)$, $C(s) = T_3 \cdot s + 1$.

20. (New) A charge rate estimating apparatus for a secondary cell, comprising:

a current detecting section capable of measuring a current flowing through the secondary cell;

a terminal voltage detecting section capable of measuring a voltage across terminals of the secondary cell;

a parameter estimating section that calculates an adaptive digital filtering using a cell model in a continuous time series shown in an equation (1) estimates all of parameters at one time, the parameters corresponding to an open-circuit voltage V_0 which is an offset term of the equation (1) and coefficients of $A(s)$, $B(s)$, and $C(s)$ which are transient terms; and

a charge rate estimating section that estimates the charge rate from a previously derived relationship between an open-circuit voltage and a charge rate of the secondary cell, and the open-circuit voltage V_0 ,

$$V = \frac{B(s)}{A(s)} \cdot I + \frac{1}{C(s)} \cdot V_0 \quad \text{--- (1),}$$

wherein s denotes a Laplace transform operator, $A(s)$, $B(s)$, and $C(s)$ denote poly-nominal functions of s ,

Wherein the open-circuit voltage V_0 of the cell model in the continuous time series shown in the equation (1) is approximated by means of an equation (2) to provide an equation (3) and the adaptive digital filter calculation is carried out using the equation (3) and equivalent equation (4), h is estimated in at least equation (4), the estimated h is substituted into equation (2) to derive an open-circuit voltage V_0 , and the charge rate is estimated from the previously derived relationship between an open-circuit voltage and a charge rate of the secondary cell and the open-circuit voltage V_0 ,

$$V_0 = \frac{h}{s} \cdot I \quad \text{--- (2)}$$

Where equations (3) and (4) do not include the open-circuit voltage V_0 , but are product and addition equations relating V and I .

21. (New) A charge rate estimating method for a secondary cell as claimed in claim 14, wherein the cell model is calculated from an equation (6),

$$V = \frac{K \cdot (T_2 \cdot s + 1)}{T_1 \cdot s + 1} \cdot I + \frac{1}{T_3 \cdot s + 1} V_0 \quad \text{wherein } K \text{ denotes an internal}$$

resistance of the secondary cell, T_1 , T_2 , and T_3 denote time constants, $1/G_1(s)$ denotes a low pass filter having a third order or more, and $1/G_2(s)$ denotes another low pass filter having a second order or more.